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RESPONSE OF SEVERAL VERTICAL ARRAY PROCESSORS

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AIR FORCE TECHNICAL APPLICATIONS CENTER
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By

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TELEDYNE, INC.

Under

Project VELA UNIFORM

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Nuclear Test Detection Office
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RESPONSE OF SEVERAL VERTICAL ARRAY PROCESSORS

SEISMIC DATA LABORATORY REPORT NO. 212

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ABSTRACT

Several of the simplest vertical array processors were evaluated by means of frequency-wavenumber spectral analysis. The processors analyzed were beamed sum, multichannel deghost, and the fan filter. Adequate responses were obtained in the specified signal pass-band for all of the processors. Considerable differences between the processors were observed in the dead-band, especially at low wavenumbers corresponding to surface wave components in the noise. The best dead-band response was obtained for the fan filter using a spacing with uphole time between instruments of .1 seconds from the top to the bottom of the well.

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PROCEDURE

The SDL frequency-wavenumber analysis program VFKSPTRM (1966) was used to calculate the response of several simple processors for vertical arrays. The impulse responses of the filters as applied to each channel was subjected to frequency-wavenumber analysis. This implies an equal and simultaneous impulsive input to each channel.

Each processor involves a beamed sum of P-waves based on normal moveout times for vertical compressional waves. The multichannel deghoster and fan filter are followed by other operations designed to remove signal distortion or improve the dead-band response of the processor. The multichannel deghoster estimates the signal waveform at the surface without regard to correlated background noise. The fan filter (1967) ideally passes waves between a specified pass-band of limiting vertical phase velocities and rejects energy outside of the band.

We examined several vertical array geometries. These are specified by uphole times based on the arrival of the up-going vertical compressional wave at each instrument in the array subtracted from the arrival time at the surface. A vertical phase velocity of 6 km/sec was used for the f-k analysis.

The following table correlates the array geometry, type of processor and figure number. Each figure shows the relative power response in the f-k plane.

TABLE 1

| Fig. No. | Processor | No. of Channels | Uphole times (sec.) | Frequency Bandpass (cps) | Velocity Bandpass (km/sec) |
|-------------|------------|--------------------|-----------------------------|--------------------------------|----------------------------------|
| 1 | Beamed sum | 7 | .05,.15,.25,.35,.45,.55,.65 | All Pass | 0 |
| 2 | Beamed sum | 7 | .05,.15,.25,.35,.45,.55,.65 | .4 - 3.0 | 0 |
| 3 | Beamed sum | 7 | .00,.15,.25,.35,.45,.55,.65 | All Pass | 0 |
| 4 | Beamed sum | 6 | .15,.25,.35,.45,.55,.65 | All Pass | 0 |
| 5 | Beamed sum | 6 | .05,.15,.25,.35,.45,.55 | All Pass | 0 |
| 6 | Beamed sum | 6 | .05,.15,.25,.35,.45,.55 | 0.4 - 3.0 | 0 |
| 7 | MCdeG | 6 | .05,.15,.25,.35,.45,.55 | All Pass | 0 |
| 8 | MCdeG | 6 | .15,.25,.35,.45,.55,.65 | All Pass | 0 |
| 9 | MCdeG | 6 | .05,.15,.25,.35,.45,.55 | 0.4 - 3.0 | 0 |
| 10 | Fan Filter | 6 | .05,.15,.25,.35,.45,.55 | All Pass | 3.0-9.0 |
| 11 | Fan Filter | 6 | .05,.15,.25,.35,.45,.55 | 0.4 - 3.0 | 3.0-9.0 |
| 12 | Fan Filter | 7 | .05,.15,.25,.35,.45,.55,.65 | 0.4 - 3.0 | 3.0-9.0 |
| 13 | Fan Filter | 6 | .15,.25,.35,.45,.55,.65 | All Pass | 3.0-9.0 |
| 14 | Fan Filter | 6 | .05,.15,.25,.35,.45,.55 | All Pass | 4.5-7.5 |

RESULTS

Comparing Figure 2 and Figure 6 we see that an 18% increase in the length of the vertical array makes only slight improvement in the array response. An array with maximum uphole time of .55 sec. with 6 instruments provides an adequate response in the signal band with the power to discriminate body waves at frequencies above .7 cps.

Figures 4, 8, and 12 show the array response for equally spaced instruments placed in the lower 2/3 of the well. The apparent resolving power is inadequate between 1.0 and 1.3 cps for all of the processors analyzed. The fan filter appears to have the desired pass-band response with better dead-band rejection than the beamed sum and multichannel deghoster.

REFERENCES

- McCowan, D.W., Finite Fourier transformer theory and its application to the computation of convolutions, correlations, and spectra, Seismic Data Laboratory Report No. 168 (Revised) Teledyne, Alexandria, Va., 1966.
- Treitel, S., Shanks, J.L., Frasier, C.W., Some aspects of fan filtering, Geophysics, Vol. 32, n. 5, 1967.

TABLE 2

Symbols For the F-K Spectral Mapping

| <u>DB</u> | <u>Symbol</u> |
|-----------|---------------|
| 0-1 | 0 |
| 1.001 - 3 | 0 |
| 6-9 | 6 |
| 12-15 | 2 |
| 18-21 | 8 |
| 24-27 | . |

```

251MMHGRAM NO.      3          80, 41 CHANNEL = 2
SAMPLING RATE = 80.00      STARTING POINT = 800      TOTAL POINTS = 120
TIME SUMMAR OF SMOOTHING TIME = 0

```

| CHANNEL ID | SCALE FACTOR | DEPTH |
|------------|--------------|-------|
| DM1 | 1.00 | .382 |
| DM2 | 1.00 | .908 |
| DM3 | 1.00 | 1.800 |
| DM4 | 1.00 | 8.100 |
| DM5 | 1.00 | 2.760 |
| DM6 | 1.00 | 2.308 |
| DM7 | 1.00 | 2.800 |

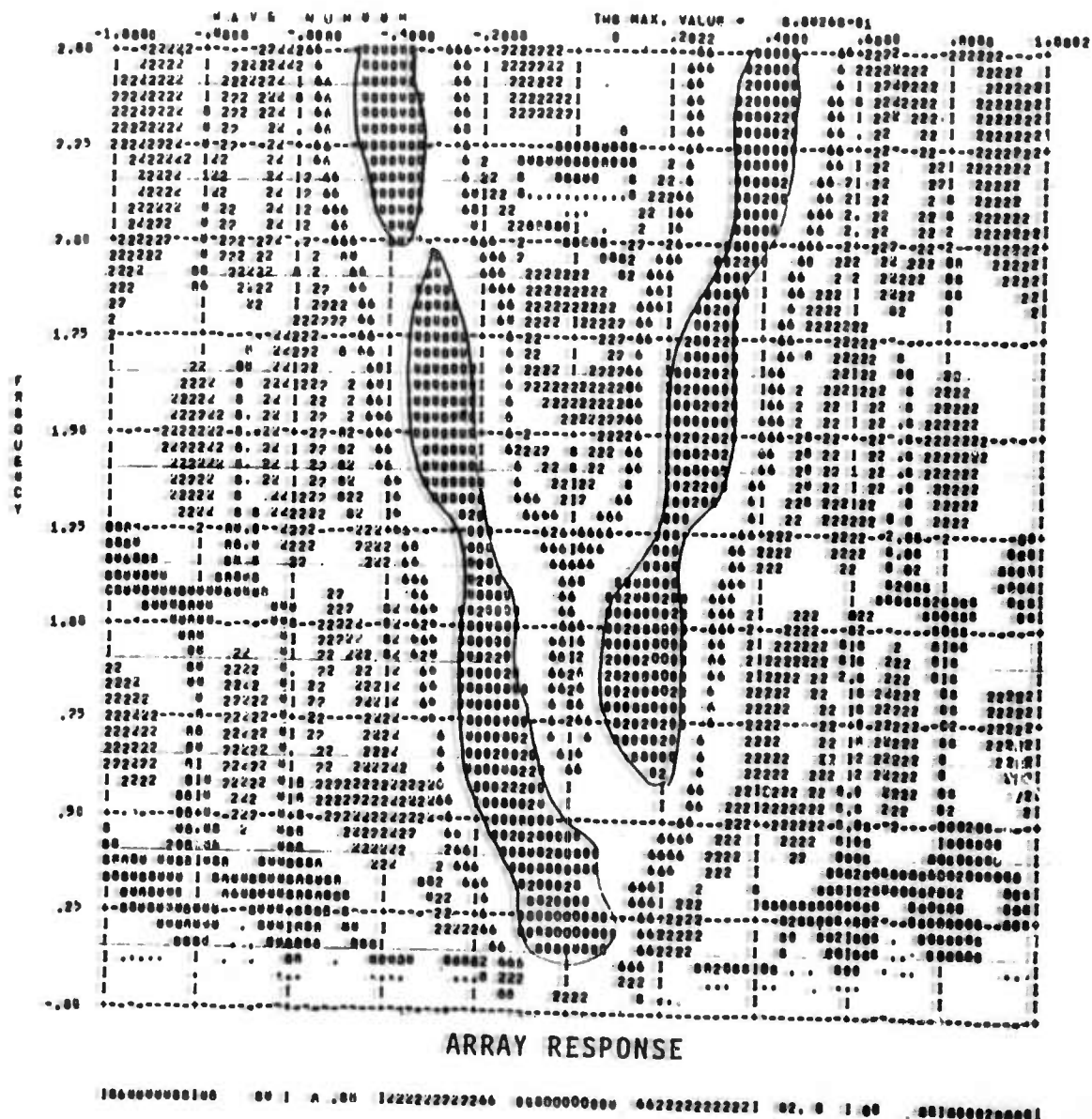


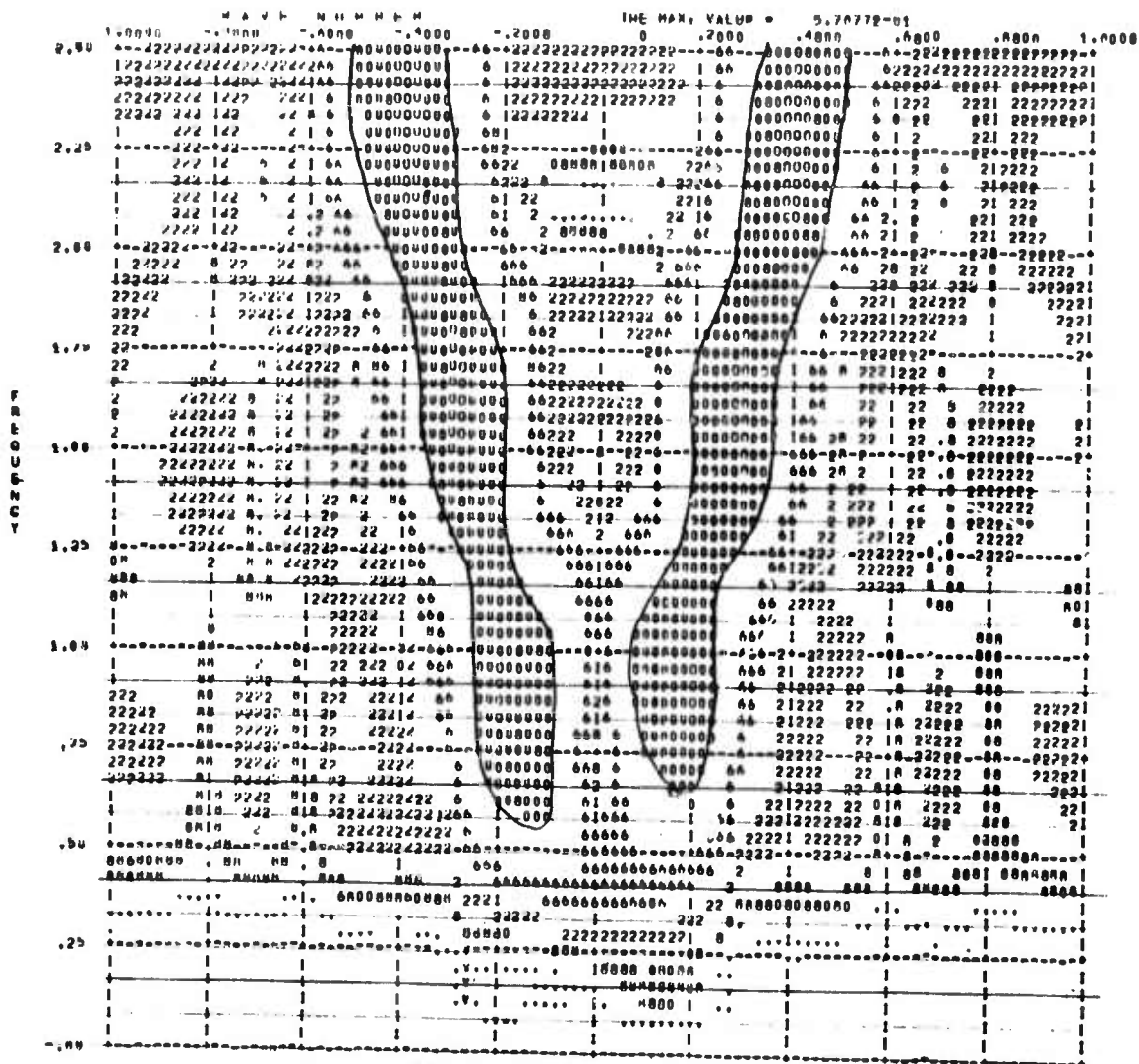
Figure 1. Beamed Sum

```

#1300016M AM, =          J              NO. OF CHANNEL = /
SAMPLE RATE = 24-40      SLALING MODELS = 000    TOTAL POINTS = 198
JOB NAME OF SAVING FILE = 0

```

| CHANNEL ID | SCALE FACTOR | HEIGHT |
|------------|--------------|--------|
| 001 | 1.00 | .300 |
| 002 | 1.00 | .900 |
| 003 | 1.00 | 1.500 |
| 004 | 1.00 | 2.100 |
| 005 | 1.00 | 2.700 |
| 006 | 1.00 | 3.300 |
| 007 | 1.00 | 3.900 |



ARRAY RESPONSE

[illegible]

Figure 2. Beamed Sum

VFKSPTRM

SEISMOGHAM MD. •

5

NO. OF CHANNEL • 7

SAMPLING RATE • 20.00

STARTING POINT • 500

TOTAL POINTS • 190

THE NUMBER OF SMOOTHING TIME • 0

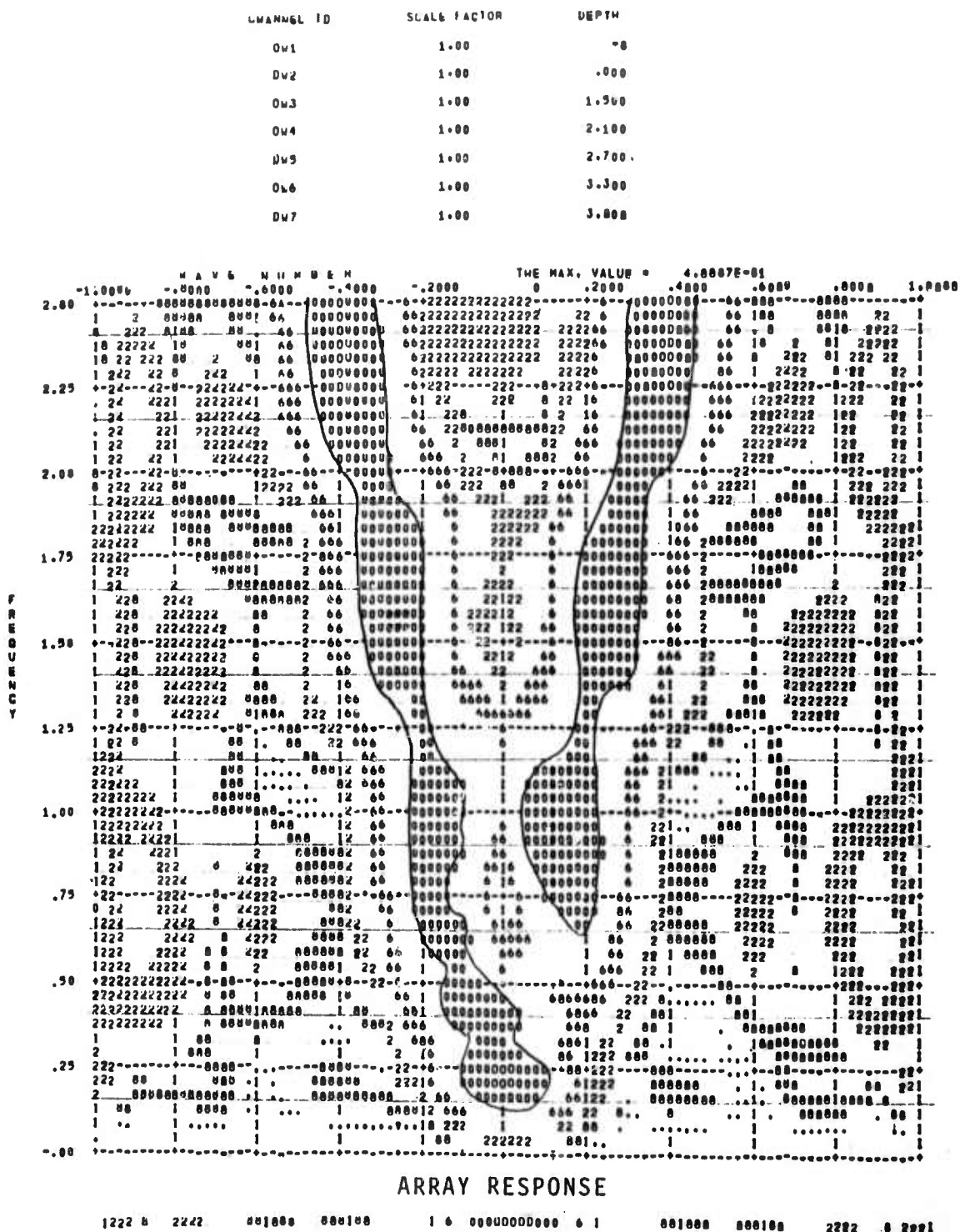
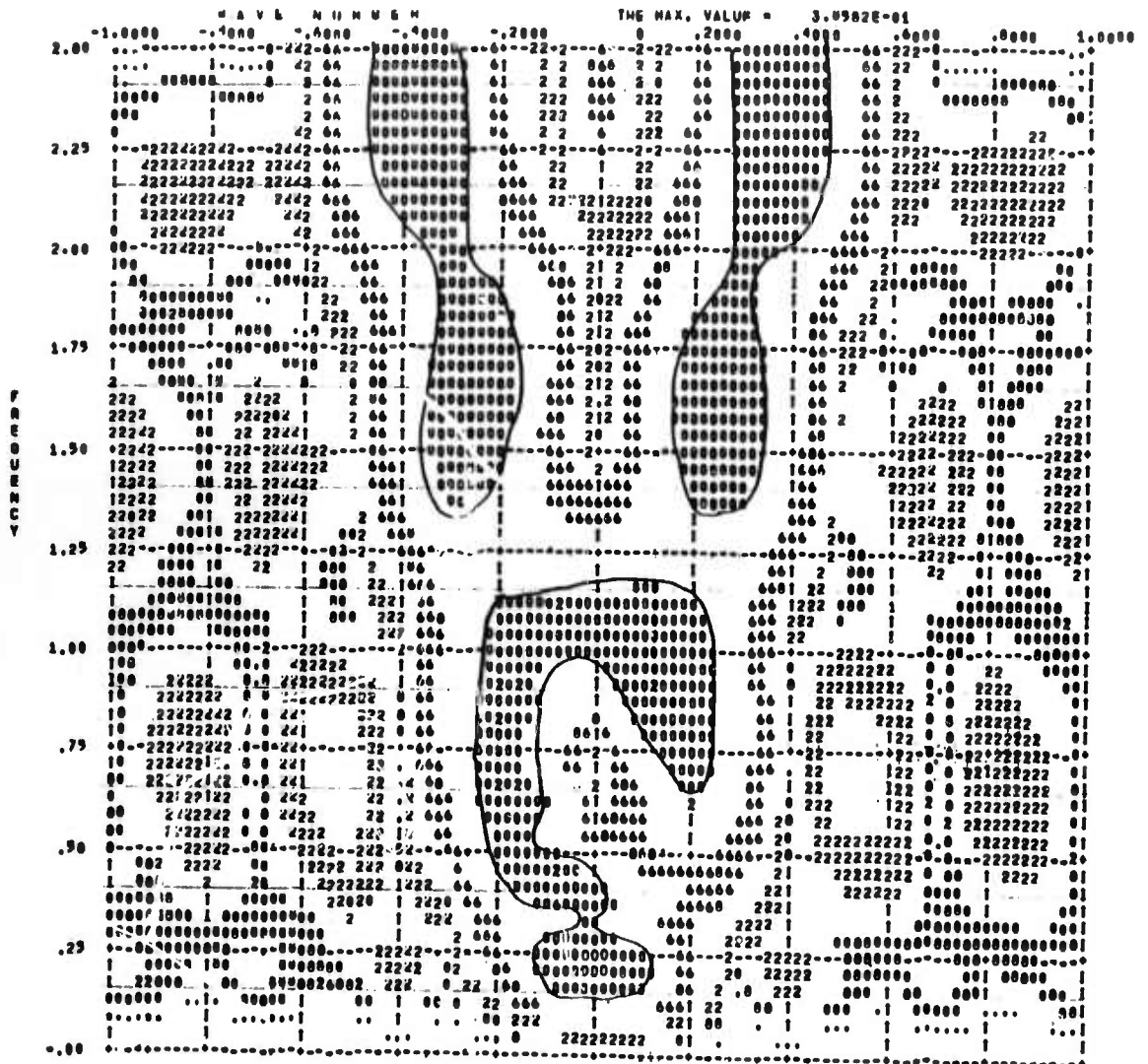


Figure 3. Beamed Sum

VISUPTM

SEISMIC STATION NO. = 2 NO. OF CHANNEL = 6
 SAMPLING RATE = 20.00 STARTING POINT = 000 TOTAL POINTS = 120
 THE NUMBER OF SHORTENING TIME = 0

| CHANNEL ID | SCALE FACTOR | DEPTH |
|------------|--------------|-------|
| DU1 | 1.00 | .900 |
| DU2 | 1.00 | 1.900 |
| DU3 | 1.00 | 0.100 |
| DU4 | 1.00 | 2.700 |
| DU5 | 1.00 | 3.300 |
| DU6 | 1.00 | 3.900 |



ARRAY RESPONSE

1 000 100 000000 222222 2 16 000000000000 61 2 222222 000000 30, 000 1

Figure 4. Beamed Sum

NO. OF CHANNEL • •

SAMPLING RATE = 20.00 ... STARTING POINT = 000 ... TOTAL POINTS = 120

THE NUMBER OF SHOOTING TIME • 0

| CHANNEL ID-- | SCALE FACTOR | DEPTH |
|--------------|--------------|-------|
| D01 | 1.00 | .300 |
| D02 | 1.00 | .900 |
| D03 | 1.00 | 1.500 |
| D04 | 1.00 | 2.100 |
| D05 | 1.00 | 2.700 |
| D1A | 1.00 | 3.300 |

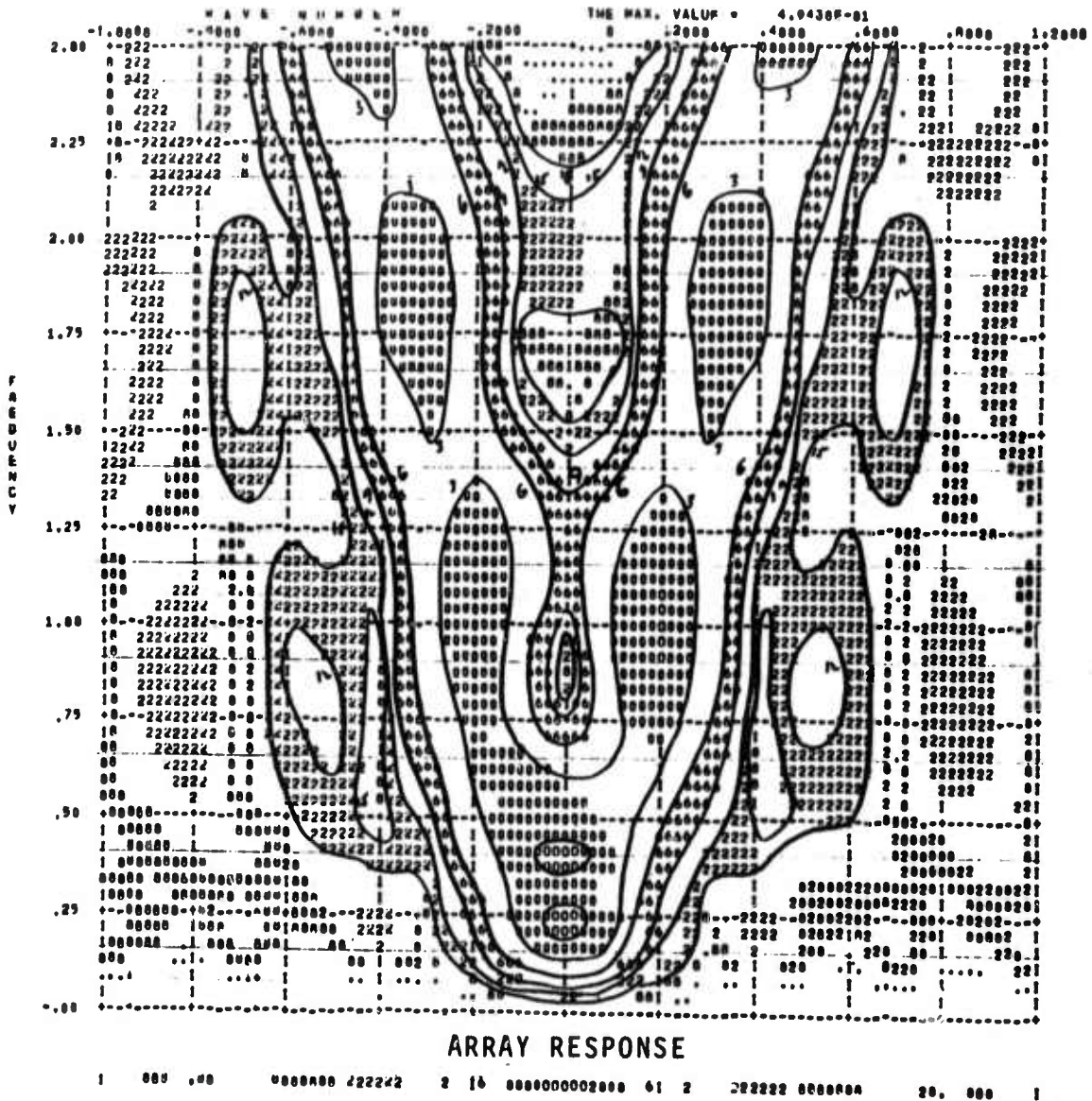
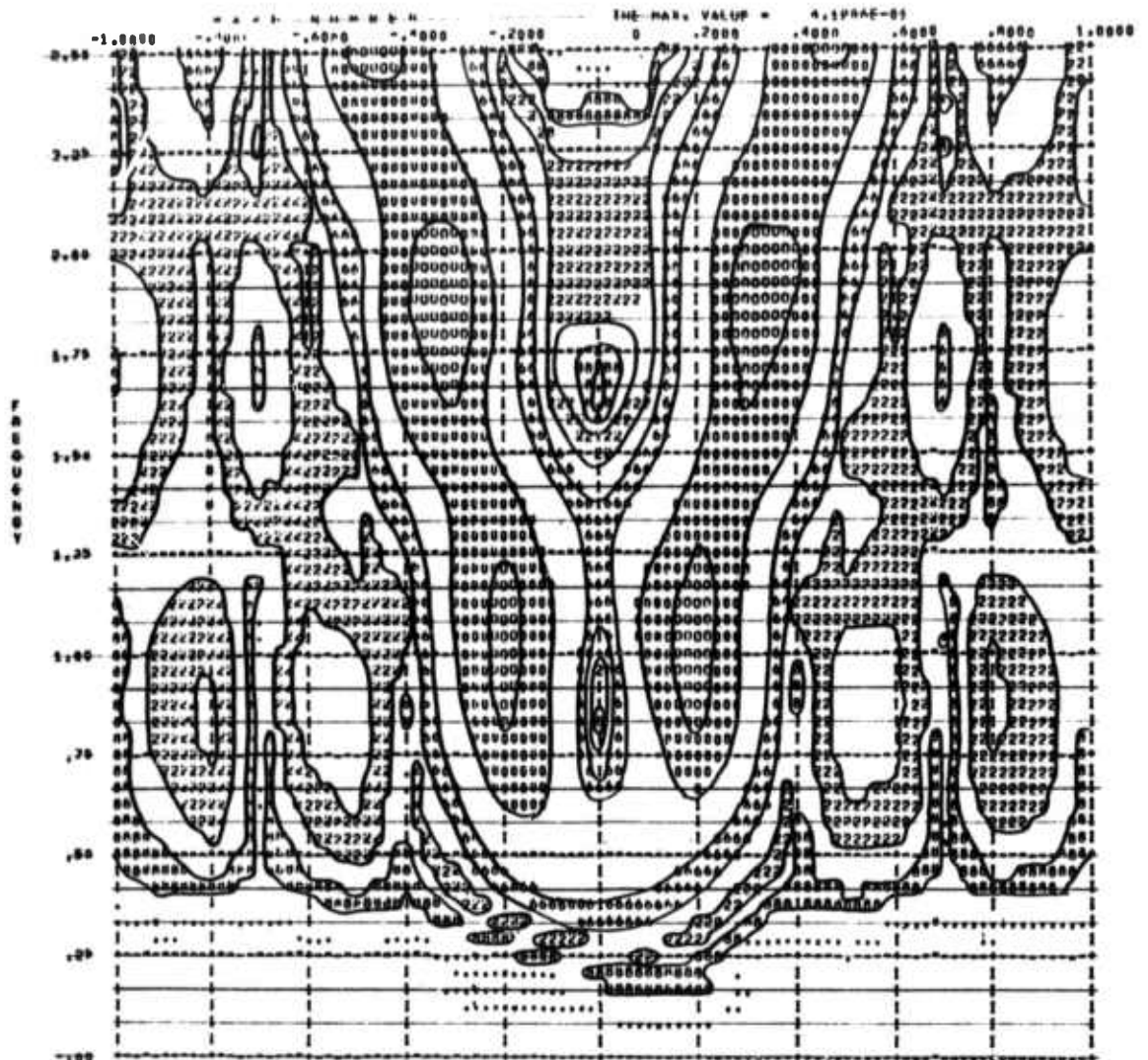


Figure 5. Beamed Sum

OF SAMPLING TIME "A" "A" NO. OF CHANNEL "A"
 SAMPLING TIME "A" "A" SLANTING POINT "A" "A" TOTAL POINTS "A"
 THE NUMBER OF SAMPLING TIME "A"

| DATE | STATE | AMOUNT |
|------|-------|--------|
| 11/1 | 1.00 | 1.300 |
| 11/2 | 1.00 | 1.900 |
| 11/3 | 1.00 | 1.500 |
| 11/4 | 1.00 | 2.100 |
| 11/5 | 1.00 | 2.700 |
| 11/6 | 1.00 | 3.300 |



ARRAY RESPONSE

1 000 .00 000000 222242 2 10 000000000000 01 2 222222 000000 00. 000 1

Figure 6. Beamed Sum

VFROPTNM

SEIGNORIAN NO. = 1

NO. OF CHANNEL = 6

SAMPLING RATE = 20.00

STARTING POINT = 500

TOTAL POINTS = 120

THE NUMBER OF SMOOTHING LINE = 0

| CHANNEL ID | SCALE FACTOR | DEPTH |
|------------|--------------|-------|
| DM1 | 1.00 | .300 |
| DM2 | 1.00 | .900 |
| DM3 | 1.00 | 1.000 |
| DM4 | 1.00 | 2.100 |
| DM5 | 1.00 | 2.700 |
| DM6 | 1.00 | 3.300 |

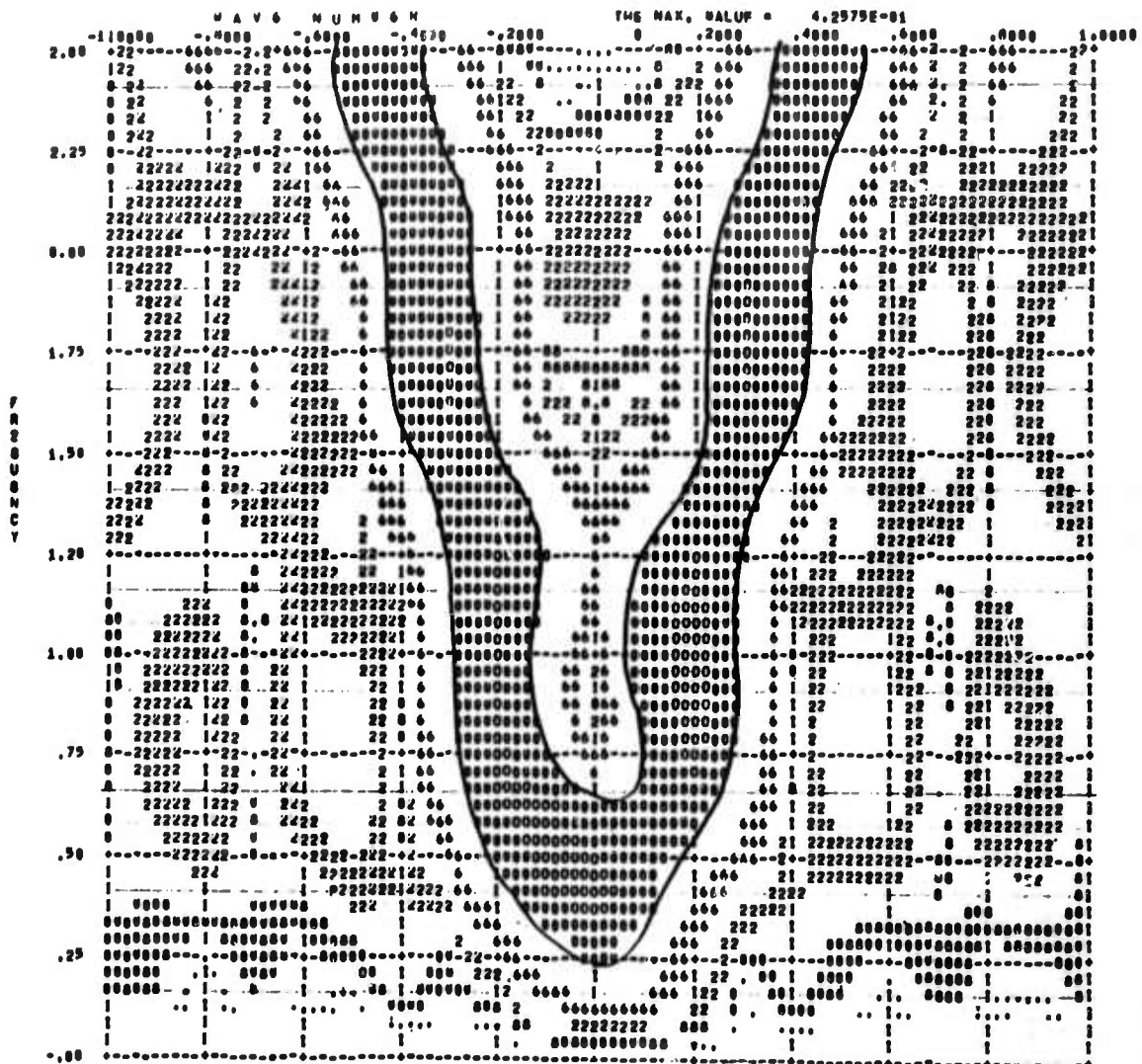


Figure 7. MCdeG

VIRKSIAM

BOJHNGHAM NO. = 2 NR. OF CHANNEL = 6
 SAKPLING HAIS = 20.00 STARTING POINT = 800 TOTAL POINTS = 120
 THE MINIMUM OF SHOOTING TIME = 0

| CHANNEL ID | SCALE FACTOR | DEPTH |
|------------|--------------|-------|
| DW1 | 1.00 | .000 |
| DW2 | 1.00 | 1.500 |
| DW3 | 1.00 | 2.100 |
| DW4 | 1.00 | 2.700 |
| DW5 | 1.00 | 3.300 |
| DW6 | 1.00 | 3.900 |

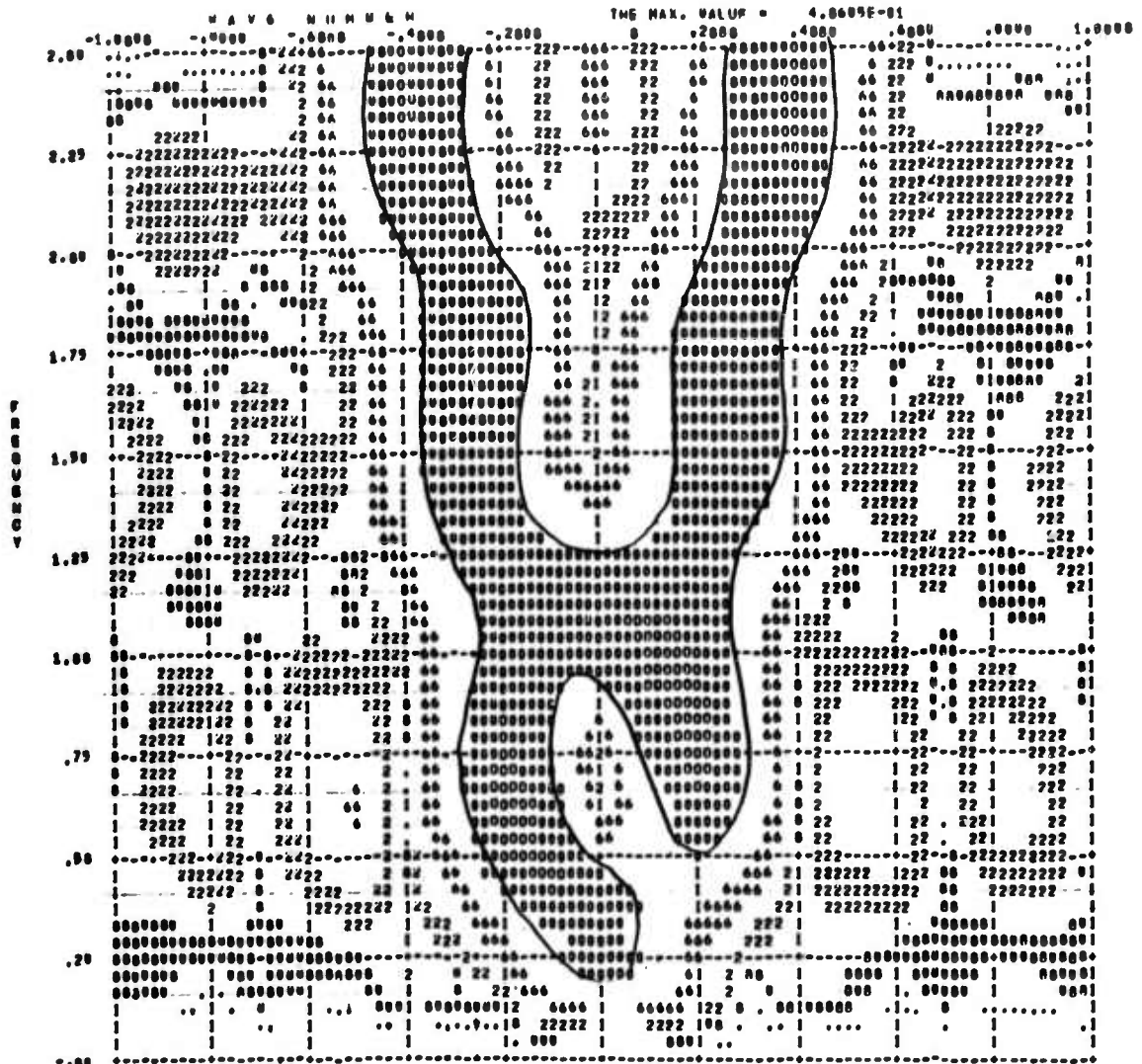
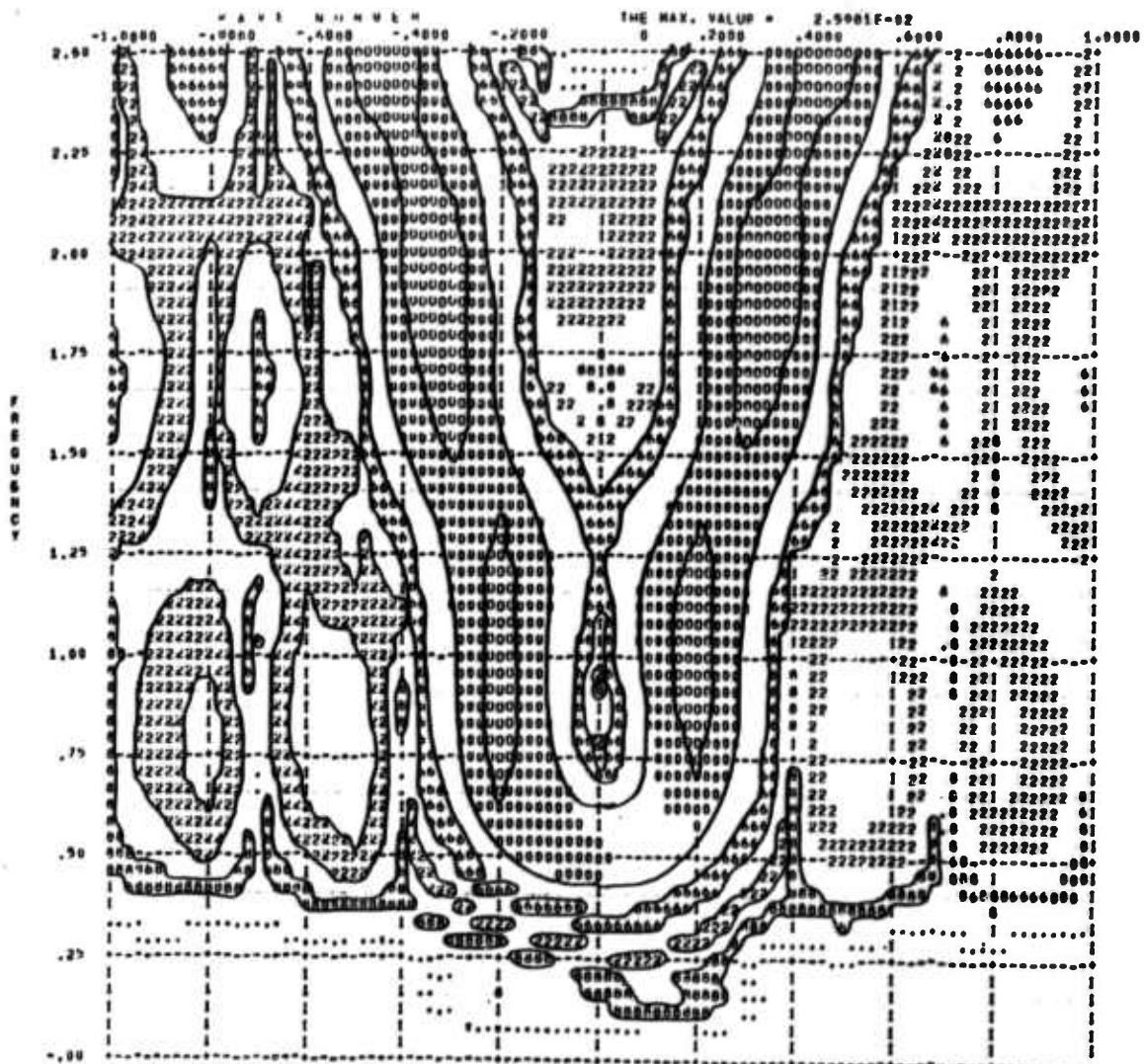


Figure 8. MCdeG

VIRSPINN

BEIRINGHAM NO. = 1 NO. OF CHANNEL = 4
 SAMPLING RATE = 20.00 HANTING POINT = 500 TOTAL POINTS = 120
 THE NUMBER OF SMOOTHING TIME = 0

| CHANNEL ID | SCALE FACTOR | DEPTH |
|------------|--------------|-------|
| D01 | 1.00 | .300 |
| D02 | 1.00 | .900 |
| D03 | 1.00 | 1.500 |
| D04 | 1.00 | 2.100 |
| D05 | 1.00 | 2.700 |
| D06 | 1.00 | 3.300 |



ARRAY RESPONSE

1 000 .00 000000 22222 2 10 000000000000 01 2 222222 000000 00. 000 1

Figure 9. MCdeG

VFROPTIM

BEIDHNGHAM NO. = 1
 NO. OF CHANNEL = 6
 SAMPLING RATE = 20.00 STARTING POINT = 400 TOTAL POINTS = 120
 THE NUMBER OF SHOOTING TIME = 0

| CHANNEL ID | SCALE FACTOR | DEPTH |
|------------|--------------|-------|
| DU1 | 1.00 | .300 |
| DU2 | 1.00 | .900 |
| DU3 | 1.00 | 1.500 |
| DU4 | 1.00 | 2.100 |
| DU5 | 1.00 | 2.700 |
| DU6 | 1.00 | 3.300 |

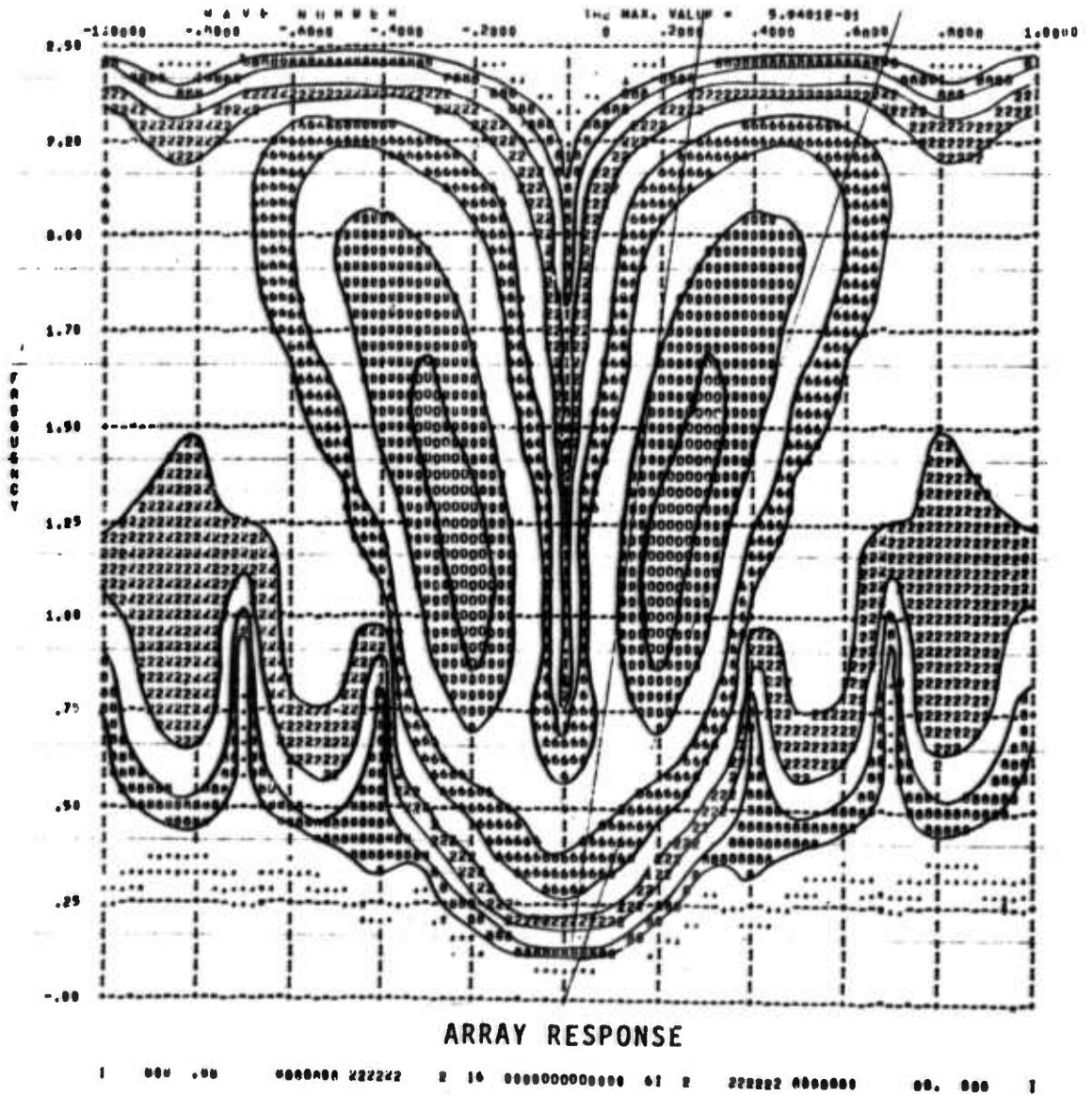


Figure 10. Fan Filter

SEISMOGRAM NO. = 1 NO. OF CHANNEL = 6
SAMPLING RATE = 20.00 STARTING POINT = 490 TOTAL POINTS = 125
THE NUMBER OF SHOOTING TIME = 8

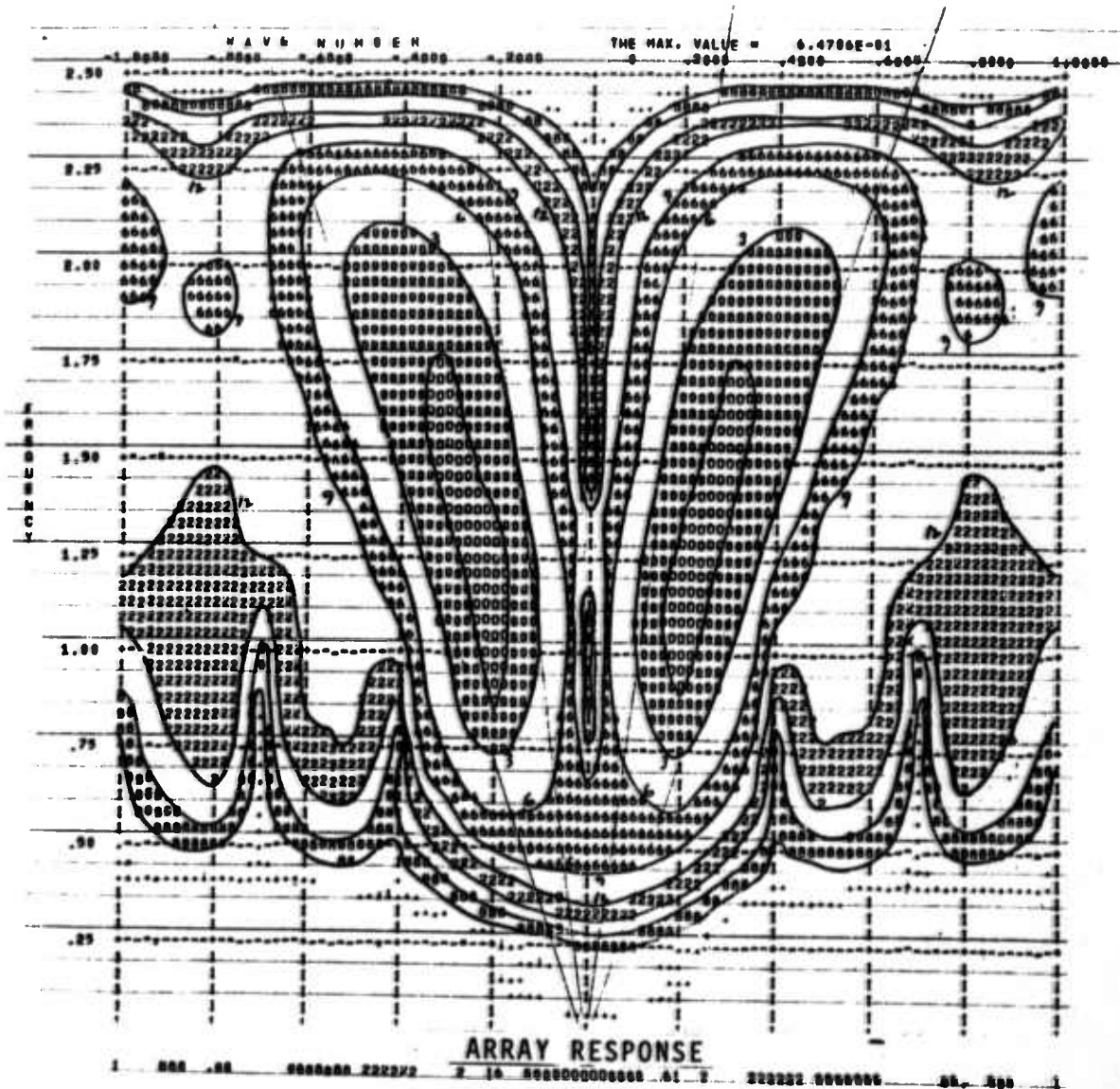
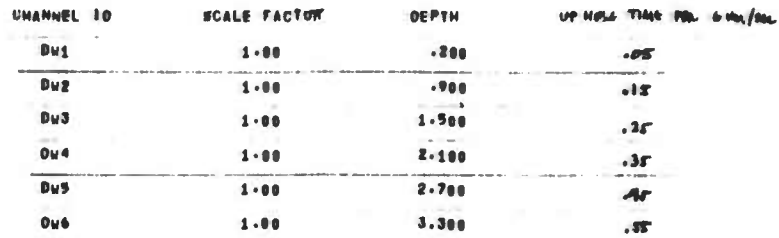
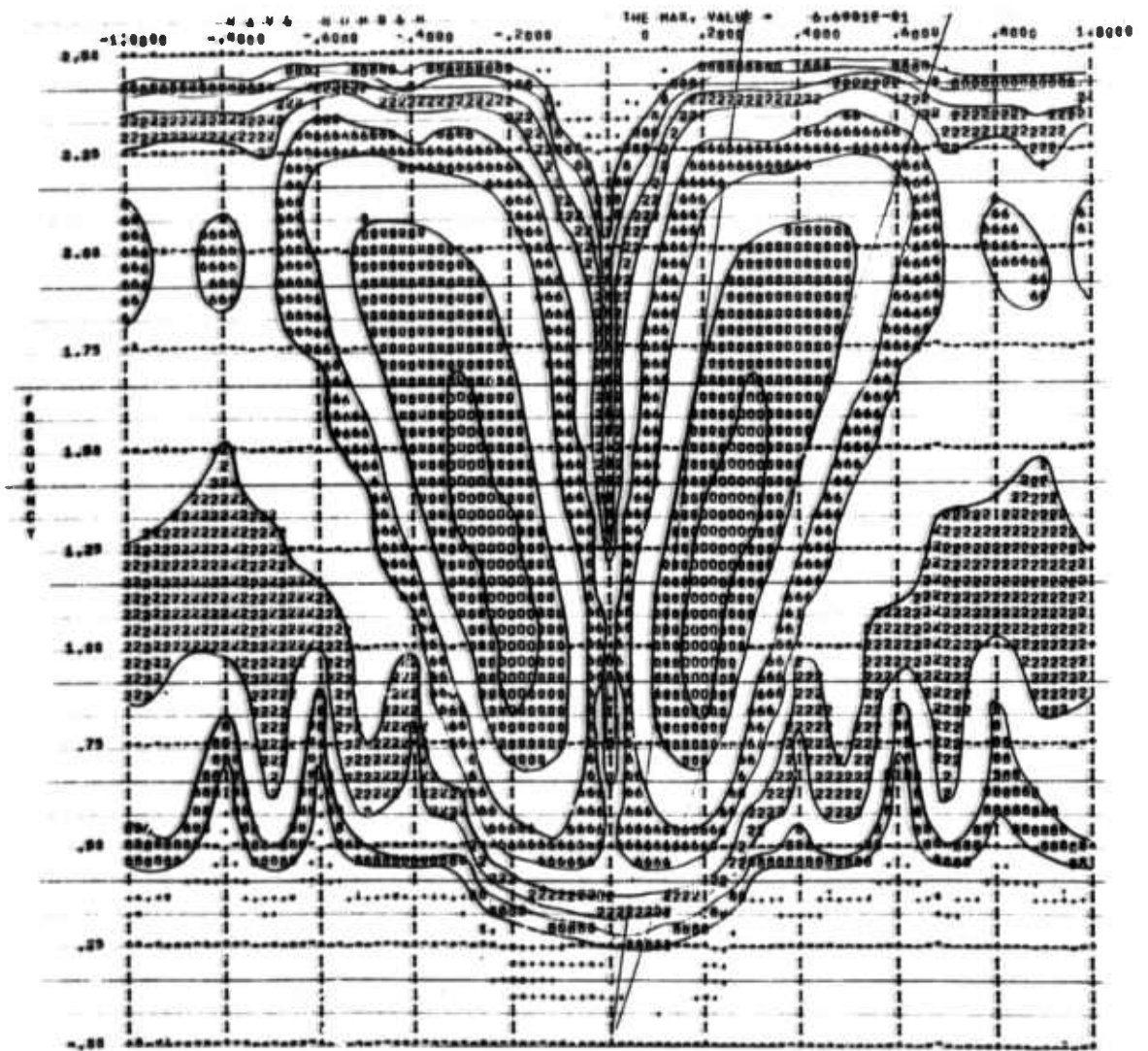


Figure 11. Fan Filter

VIASTIM

SCHEMATIC NO. = 1
 NO. OF CHANNEL = 7
 SAMPLING RATE = 20.00 STARTING POINT = 400 TOTAL POINTS = 100
 THE NUMBER OF SMOOTHING TIME = 0

| CHANNEL ID | SCALE FACTOR | DEPTH | UP HOLD TIME FOR 60 HZ |
|------------|--------------|-------|------------------------|
| D01 | 1.00 | .300 | .05 |
| D02 | 1.00 | .900 | .15 |
| D03 | 1.00 | 1.500 | .25 |
| D04 | 1.00 | 2.100 | .35 |
| D05 | 1.00 | 2.700 | .45 |
| D06 | 1.00 | 3.300 | .55 |
| D07 | 1.00 | 3.900 | .65 |



ARRAY RESPONSE

100000000000 00 1 0.00 122222222200 0000000000 042222222221 00.0 1 00 0010000000001

Figure 12. Fan Filter

VFH0PTM

SEGMENT NO. = 1 NO. OF CHANNEL = 4
 SAMPLING RATE = 20.00 STARTING POINT = 034 TOTAL POINTS = 194
 THE NUMBER OF SMOOTHING TIME = 0

| CHANNEL ID | SCALE FACTOR | OFFSET |
|------------|--------------|--------|
| Vp | 1.00 | -0.00 |
| V3 | 1.00 | 1.500 |
| V4 | 1.00 | 2.100 |
| V5 | 1.00 | 2.700 |
| V6 | 1.00 | 3.300 |
| V7 | 1.00 | 3.900 |

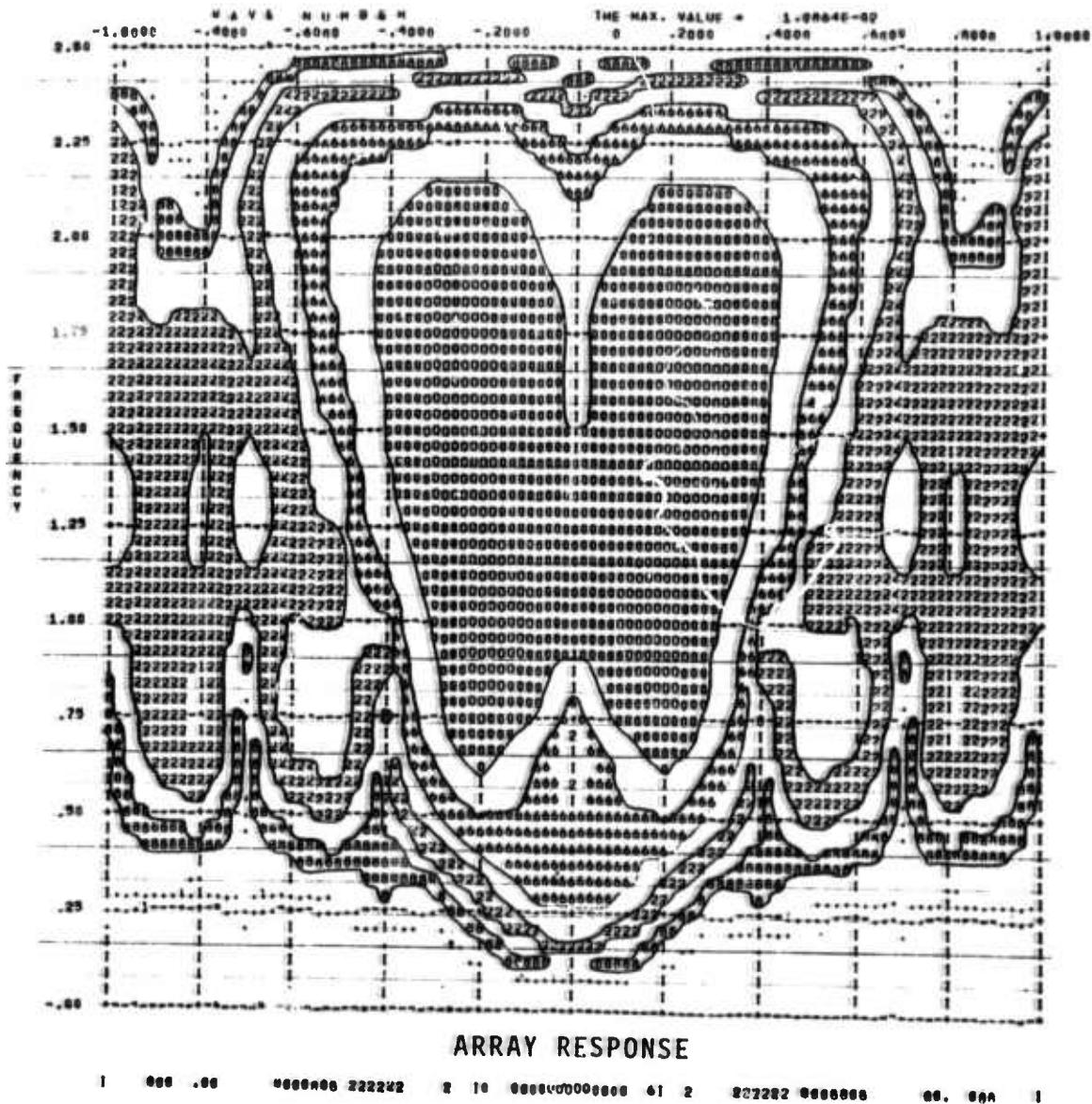
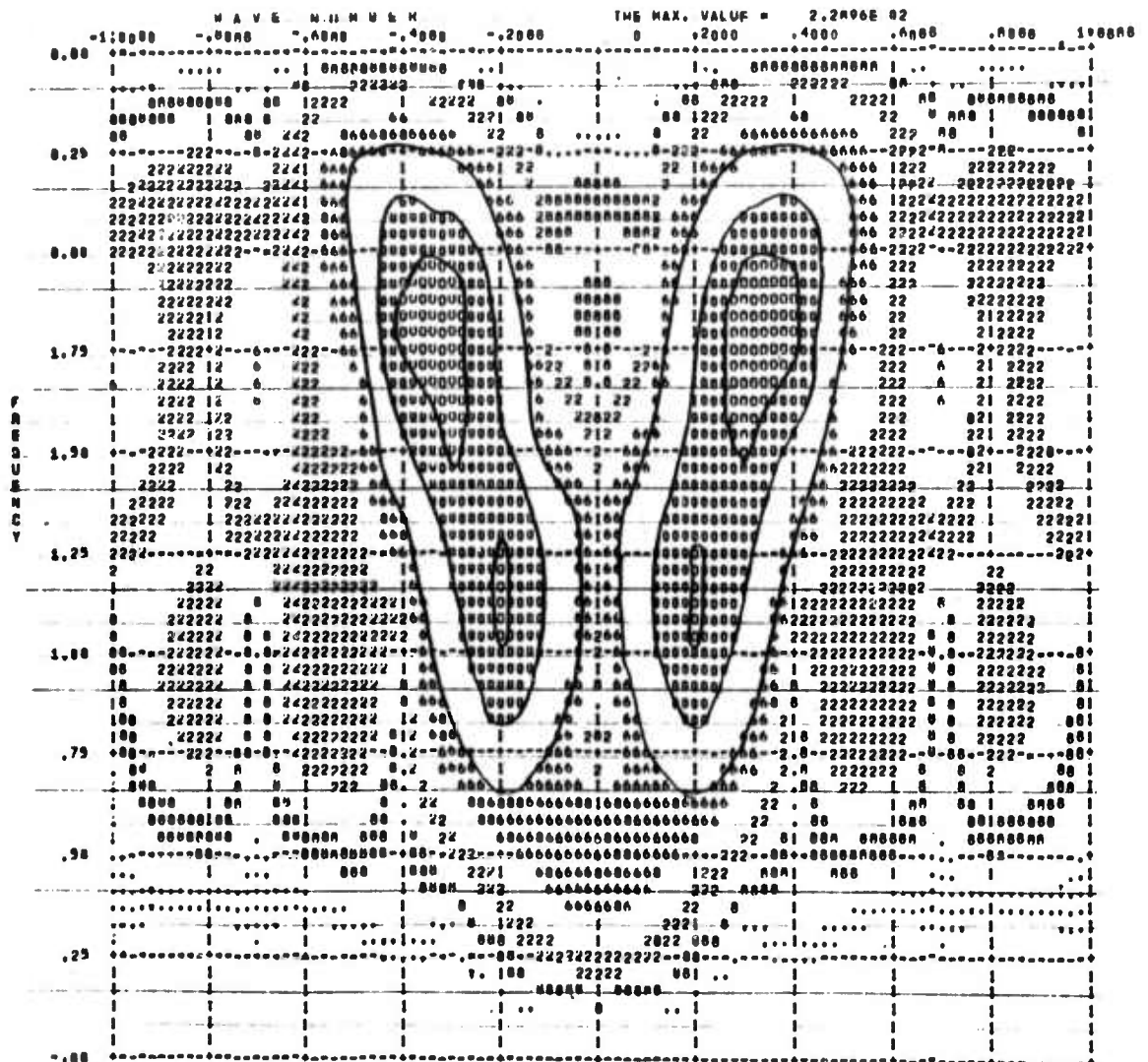


Figure 13. Fan Filter

| CHANNEL ID | SCALE FACTOR | DEPTH |
|------------|--------------|-------|
| Vp | 1.00 | .000 |
| V3 | 1.00 | 1.500 |
| VA | 1.00 | 2.100 |
| V9 | 1.00 | 2.700 |
| V6 | 1.00 | 3.300 |
| V7 | 1.00 | 3.900 |



ARRAY RESPONSE

1 000 .00 0000000 222222 2 10 0000000000000000 01 2 222222 0000000 00. 000 1

Figure 14. Fan Filter

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14. KEY WORDS

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Frequency-Wavenumber Spectral Analysis
Beamed Sum
Multichannel Degghost

Fan Filter

Unclassified

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